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## Abstract

In the exploration and production activities within the petroleum industry, the presence of corrosive gases, such as CO<sub>2</sub> and H<sub>2</sub>S, in hydrocarbon reservoirs poses significant challenges. Depending on their concentrations, these gases can jeopardize worker safety, cause equipment damage, and potentially render a project economically unviable. In the Santos Basin, Brazil, there is a notable presence of wells with concentrations of CO<sub>2</sub> exceeding 5 %, even reaching up to 80 % in certain areas [1]. Among the various techniques employed for CO<sub>2</sub> separation, ceramic membranes have emerged as a promising technology for upstream applications. These membranes exhibit unique structural and functional properties, offering a viable alternative to conventional methods like amine-based systems [2-3].

Ceramic membranes, characterized by their multilayered structure, encompassing macroporous support, mesoporous intermediate, and microporous separation layers, provide an attractive solution for selective  $CO_2$  removal. The advantages of ceramic membranes lie in their high permeation rates and molecular sieving, allowing smaller gas molecules to pass through while obstructing larger ones. This unique property contributes to the membranes' high selectivity and relatively high permeability. Furthermore, the fabrication of ceramic membranes through processes like sol-gel ensures versatility in tailoring the pore sizes and structures, enhancing the membranes' efficiency for  $CO_2$  separation from natural gas [2].

Ceramic membranes were developed at Federal University of Minas Gerais (UFMG) for CO<sub>2</sub> separation in natural gas, emphasizing tailored properties for high pressure processing. UFMG ceramic membranes were produced by depositing sol-gel silica solutions onto  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> mono-channel tubular supports (OD  $\approx$  9 cm), followed by the appropriate thermal treatment. The alumina ceramic mass of the supports received additions of TiO<sub>2</sub> (1 %, 3 %, and 5 % wt.) to enhance the mechanical strength of the ceramic membranes.

Single-gas permeation tests (CO<sub>2</sub>, N<sub>2</sub>, and CH<sub>4</sub>) were performed at room temperature to determine the permeance of UFMG ceramic membranes using Eq. (1), where V<sub>p</sub> is the permeate flow rate (cm<sup>3</sup><sub>(STP)</sub>/s), A<sub>m</sub> is the membrane separation area (cm<sup>2</sup>), P<sub>F</sub> and P<sub>P</sub> are the pressure (cm·Hg) in feed and permeate side, respectively. The ideal selectivity or ideal permselectivity ( $\alpha^*_{A/B}$ ) was calculated by the ratio of permeances for gas pairs as per Eq. (2). The mechanical strength of the membranes was assessed through three-point bending tests (30 mm span) using a universal mechanical testing machine (Instron, EMIC 2310) with a compression rate of 0.5 mm/min.

$$\rho_{A} = V_{P} / (A_{m} . (P_{F} - P_{P}))$$
(1)

$$\alpha_{A/B}^* = \rho_A / \rho_B \tag{2}$$

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According to the single-gas permeation tests, the UFMG ceramic membranes exhibited a high flux of carbon dioxide. A CO<sub>2</sub> permeance of  $1.1 \times 10^{-6}$  mol/m<sup>2</sup>·s·Pa was achieved at a feed pressure of 9 bar ( $9.0 \times 10^{5}$  Pa) with a  $\Delta$ P of 2.1 bar ( $2.1 \times 10^{5}$  Pa). The CO<sub>2</sub> permeance of the UFMG ceramic membrane is significantly higher than that of polymeric membranes commonly employed in gas separations, exceeding a typical polymeric membrane with a permeance of 1,500 Barrer ( $10^{-7}$  mol/m<sup>2</sup>·s·Pa) by one order of magnitude. For this same condition the nitrogen and methane permeance were 1.5 x  $10^{-7}$  mol/m<sup>2</sup>·s·Pa and  $1.1 \times 10^{-7}$  mol/m<sup>2</sup>·s·Pa respectively.

The results of ideal permselectivity for the gas pairs  $CO_2/N_2$  and  $CO_2/CH_4$  of UFMG ceramic membranes are presented in Tab. 1. The UFMG ceramic membrane showed a  $CO_2/CH_4$  permselectivity of 9.7, indicating its efficiency in  $CO_2$ separation from natural gas. Also, the results showed that the permselectivity obtained for the pair  $CO_2$  and  $CH_4$  is higher when compared to the  $CO_2$  and  $N_2$  ( $\alpha^*_{CO_2/CH_4} = 7$ ). This occurs due to the larger difference in size between carbon dioxide and methane, when comparing to carbon dioxide and nitrogen, which confirms sieving effect present in the membranes due to its pore sizes.





Tab. 1 - Ideal permselectivity for the gas pairs CO<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/CH<sub>4</sub> of UFMG ceramic membranes.

P <sub>feed</sub> [bar]	ΔP [bar]	$\alpha^*_{CO_2/N_2}$	$\alpha^*_{CO_2/CH_4}$
2	1.0	3.1	4.5
4	1.3	4.7	6.7
6	1.6	5.8	8.2
8	1.9	6.7	9.3
9	2.1	7.0	9.7

The ceramic support plays a pivotal role in providing mechanical strength to ceramic membranes, directly influencing their robustness. It is evident that the mechanical strength of the support is directly correlated with the mechanical strength of the UFMG ceramic membranes derived from it. The mechanical strength of UFMG ceramic membranes, manufactured from ceramic supports with different chemical compositions and thermal treatments, are shown in Tab. 2. The findings indicate that the mechanical properties of UFMG ceramic membranes can be tailored through the introduction of TiO<sub>2</sub> and variations in the thermal treatment temperature of the supports. These adjustments facilitate the optimization of the mechanical characteristics of the membranes, enhancing their strength and durability. The results suggest that UFMG ceramic membranes exhibit a remarkable capacity to withstand high loads. This implies that these membranes can be successfully employed in gas separation processes, even under extremely high-pressure conditions, reaching up to 2900 bar. This study makes a contribution to the understanding and enhancement of the mechanical performance of ceramic membranes, expanding their potential applications in gas separation processes within the oil and gas industry.

Tab. 2 - Mechanical strength of UFMG ceramic membranes according to the composition and sintering temperature of the support.

TiO <sub>2</sub> loading		Ceramic support mechanical strength [MPa]				
	1,300 °C	1,400 °C	1,500 °C	1,600 °C		
0 % wt.	11.9 ± 7.1	34.6 ± 7.3	54.4 ± 22.9	73.3 ± 19.4		
1 % wt.	48.2 ± 4.9	109.6 ± 27.8	133.8 ± 20.4	206.8 ± 85.4		
3 % wt.	62.7 ± 19.1	142.5 ± 15.0	207.0 ± 10.2	234.5 ± 128.7		
5 % wt.	55.8 ± 32.5	136.1 ± 8.7	192.4 ± 20.2	296.3 ±24.1		

## References

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